### **STORM DRAINAGE REPORT**

# PROPOSED RESIDENCE 3404 72<sup>ND</sup> PL. S.E. MERCER ISLAND, WA

Prepared for

RKK Construction 3056 70<sup>th</sup> Avenue SE Mercer Island, WA 98040

July 2020

Darla Guerrero, P.E. 15020 S.E. 46<sup>TH</sup> Street Bellevue, WA 98006 Tel: 425-743-4307

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PROJECT SITE

# **VICINITY MAP**

### PROJECT DESCRIPTION

#### 1.1 SITE LOCATION

The subject property, 3404 72<sup>nd</sup> Place S.E., is located on the east side of 72<sup>nd</sup> Place S.E. and just east of S.E. 34th Street. (See Vicinity Map). The site will be developed with the construction of a single family residence with driveway, patio, walkway, and landscaping on the lot.

#### 1.2 EXISTING CONDITIONS

The site is presently developed with a single family residence and a gravel driveway. (See Figure 1.1 Existing Conditions Exhibit).

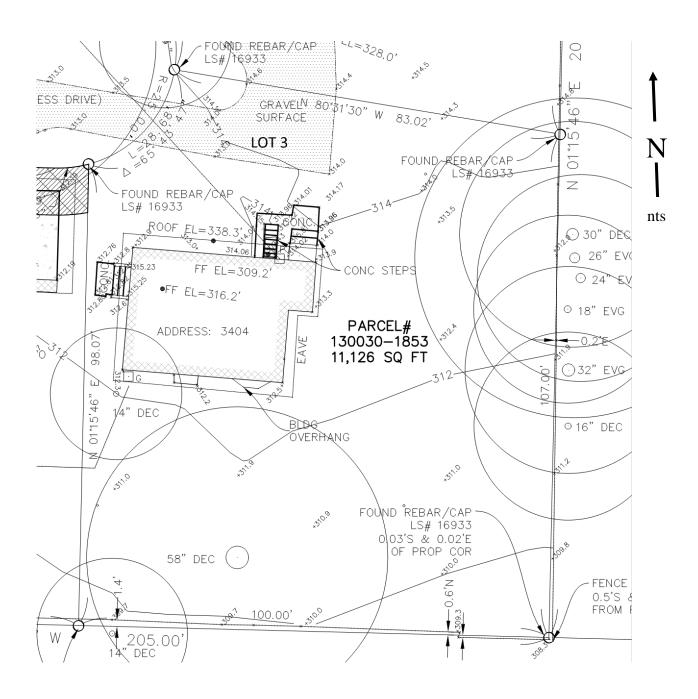
The lot slopes from the north to the south property line of the parcel. Slopes vary, but generally are approximately 5 to 6 percent. Soils are Vashon Recessional Outwash material (See Geotechnical Report Appendix A).

Storm runoff will enter the property from the developed adjacent lot to the north by overland flow. No flow will enter from the west, east or the south as contours fall off in those directions.

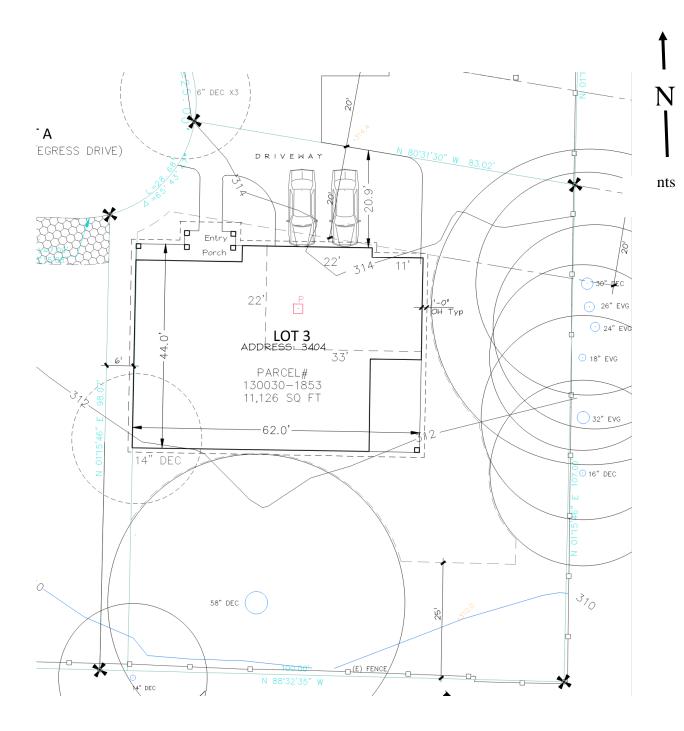
#### 1.3 DEVELOPED CONDITIONS

Lot development will include removal of existing structure and clearing and grading of the lot for the construction of a new single-family residence, driveway, patio, walkway, and landscaping. The new impervious area of the developed lot is 4,300 sf (See Figure 1.2 Developed Conditions Exhibit).

A storm drainage system was designed and constructed to collect runoff from the impervious areas of the roof, patio, walkway, and driveway with the short plat improvements. Roof runoff will enter gutters and be directed to downspouts connected the existing detention system located on the west side of the residence. Driveway runoff will be collected in a driveway drain. Stormwater from downspouts, yard drains and the driveway drains will be conveyed to a detention system.



**Figure 1.1 Existing Conditions Exhibit** 



**Figure 1.2 Developed Conditions Exhibit** 

### MINIMUM STORMWATER REQUIREMENTS

#### 1.4 MINIMUM REQUIREMENTS (MR)

Lot development will contain 4,300 square feet of new impervious surfaces and therefore the project must comply with minimum requirements MR1 through MR5. (See Figure I-2.4.2)

#### 1.4.1 MR #1 – PREPARATION OF STORMWATER SITE PLANS

A stormwater site plan detailing the collection, conveyance, and discharge of stormwater from the site has been prepared and will be included in the building permit submittal. The stormwater site plan was prepared per the City of Mercer Island Development Services Standards. The detention system has been installed with the short plat improvement requirements.

#### 1.4.2 MR #2 – SMALL PROJECT STORMWATER SITE/PLAN REPORT

A Small Project Stormwater Site/Plan Report and a Temporary Erosion Sediment Control Plan have been prepared and will be included in the building permit submittal. The Small Project Stormwater Site/Plan Report addresses the five (5) Minimum Requirements (MR).

#### 1.4.3 MR #3 – SOURCE CONTROL OF POLLUTION

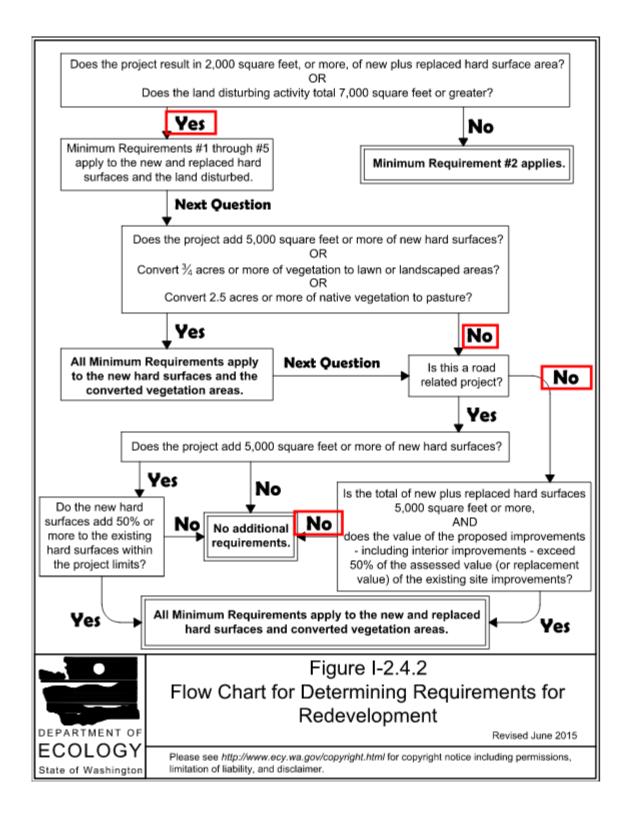
Source control BMP's are included in the SWPP Worksheet and are shown on the Temporary Erosion Sediment Control Plan. The source control BMPs are intended to prevent stormwater from coming in contact with pollutants.

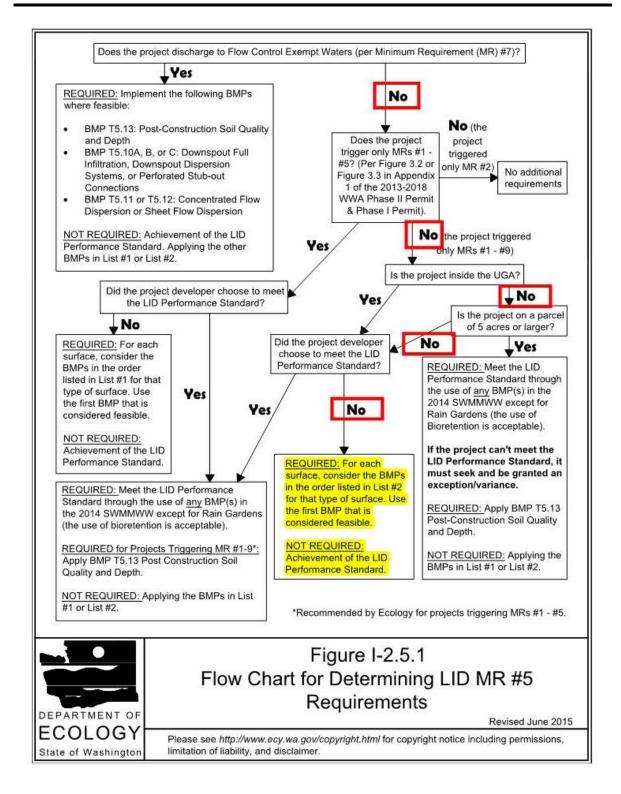
# 1.4.4 MR #4 – PRESERVATION OF NATURAL DRAINAGE SYSTEMS AND OUTFALLS

The natural drainage direction is to the south and then to the storm drain system in 72<sup>nd</sup> Place SE and has been retained. Discharge leaving the property will enter the 72<sup>nd</sup> Place SE roadway drainage system which connects to an existing storm drain system in S.E 71<sup>st</sup> Street with eventual outfall into Lake Washington. A Downstream Level One Analysis was not required for this project as detention systems were installed per the short pat requirements.

#### 1.4.5 MR #5 – ONSITE STORMWATER MANAGEMENT

This project triggers Minimum Requirements #1 through #5 and must meet the requirements in Figure I-2.5.1. No low impact development BMPs will be used on this site. The site Geotechnical Report states this site is appropriate for infiltration. (See Appendix A, Geotechnical Report)





### **ONSITE STORMWATER MANAGEMENT**

#### 1.5 TIER 1: MINIMIZE RUNOFF GENERATION

#### 1.5.1 SMART SITE DESIGN

The site development has been laid out to create minimum impact. The total impervious surface area for roof, patio, walk, and driveway is 4,300 square feet.

#### 1.5.2 PRESERVE NATIVE VEGETATION

With the exception of existing trees, there is no significant native vegetation outside the building areas. Selected existing trees will be preserved and maintained during construction.

Lawn and Landscape Areas: The site will provide Post-Construction Soil Quality and Depth in accordance with BMP T5.13 (See the TESC Plan and TESC Detail sheets). The topsoil layer shall have a minimum depth of 8-inches, mulching planting beds shall have 2-inches of organic material. The undisturbed areas will be maintained and protected during construction.

#### 1.5.3 FULL DISPERSION AND FULL INFILTRATION

Full dispersion or infiltration is not feasible per the Geotechnical Report.

The site soil is Vashon Recessional Outwash soil. City mapping shows the site is infeasible for onsite infiltration. The site Geotechnical Report states this site is not appropriate for dispersion. (See Appendix A, Geotechnical Report)

- Full Dispersion is not feasible per the Geotechnical Report.
- Full Infiltration is not feasible as the Geotechnical Report has determined the infiltration rate for each lot.
- Rain Gardens: The site is unsuitable suitable for rain gardens as the Geotechnical Report has determined the lots are not feasible for onsite infiltration.
- Downspout Dispersion is not feasible per Geotechnical Report.
- Perforated Stub-out Connection can be utilized the site is infeasible for onsite infiltration.

#### 1.5.4 AMENDED SOILS

Amended soil will be used over the disturbed areas that will be landscaped per Post-Construction Soil Quality and Depth in accordance with BMP T5.13, see the TESC plan and TESC detail sheets.

#### 1.6 TIER 2: RETAIN RUNOFF ON SITE

As discussed in full dispersion and full infiltration above, retention of runoff onsite is not a feasible option.

*Bioretention* will not be used for the same reasons listed for the Rain Gardens under Section 1.5.3 above.

Pervious pavement for the driveway will not be used for the same reasons listed above for Perforated Stub-out Connection under Section 1.5.3 above.

Rain Harvesting will not be used.

*Vegetated roof* is not a practical system due to the roof design and slope.

#### 1.7 TIER 3: INFILTRATE OR DISPERSE RUNOFF PRIOR TO DISCHARGE

As discussed above in Section 1.5.3 dispersion and infiltration are not feasible on this site per the Geotechnical Report.

### **Appendix A: Geotechnical Report**



June 3, 2019 ES-6695

#### Earth Solutions NW LLC

Geotechnical Engineering, Construction Observation/Testing and Environmental Services

RKK Construction, Inc. 3056 – 70<sup>th</sup> Avenue Southeast Mercer Island, Washington 98040

Attention:

Mr. Jason Koehler

Subject:

Infiltration Evaluation

**Levenson Property** 

3404 and 3406 - 72nd Place Southeast

Mercer Island, Washington

Reference:

Washington State Department of Ecology

2014 Stormwater Management Manual for Western Washington

Terrane

Topographic & Boundary Survey, dated April 18, 2019

M.A. Jones

Geologic Framework for the Puget Sound aquifer system, Washington and British

Columbia, 1999

United States Department of Agriculture Natural Resources Conservation Service Online Web Soil Survey (WSS) resource

Dear Mr. Koehler:

As requested, Earth Solutions NW, LLC (ESNW) has prepared this letter for the subject site. Our scope of services included subsurface exploration, infiltration testing, engineering analysis, and preparation of this letter.

#### **Project Description**

The subject site is located east of the intersection between Southeast 34<sup>th</sup> Street and 72<sup>nd</sup> Place Southeast, in Mercer Island, Washington, as illustrated on the attached Vicinity Map (Plate 1). The site consists of four adjoined residential tax parcels (King County Parcel Nos. 130030-1850, -1851, -1852, and -1853) totaling approximately 0.96 acres of land area. The property is currently developed with two single-family residences, a detached garage, a detached car port, and associated infrastructure improvements. We understand existing structures will be removed, and four new single-family residences and related improvements will be constructed.

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If the design assumptions outlined in this section are incorrect or change, or if construction conditions differ from those encountered during our fieldwork, ESNW should be contacted to review the recommendations and conclusions provided in this letter.

#### **Subsurface Conditions**

An ESNW representative observed, logged, and sampled eight test pits excavated across the subject site using a mini-trackhoe and operator provided by the client on May 7<sup>th</sup> and May 8<sup>th</sup>, 2019. The approximate locations of the test pits are depicted on Plate 2 (Test Pit Location Plan). Please refer to the attached test pit logs for a more detailed description of subsurface conditions. Representative soil samples collected at the test pit locations were analyzed in accordance with both Unified Soil Classification System (USCS) and United States Department of Agriculture (USDA) methods and procedures.

Topsoil was encountered in the upper approximate 6 to 12 inches of existing grades at the test pit locations, characterized by dark brown color, the presence of fine organic material, and small root intrusions. Surficial fill was encountered at test pit locations TP-2 and TP-5 and was restricted to the topsoil layer. Fill may also be present near existing structural improvements and along drive and access ways within the subject property. Where encountered, fill should be evaluated by ESNW at the time of construction to assess the suitability for use as structural fill and/or foundation support.

Underlying topsoil and fill, native soils primarily consisting of loose to medium dense silty sand with varying amounts of gravel (USCS: SM) were encountered. Underlying the upper silty sand layer, native soils were observed to vary amongst poorly graded sand with varying amounts of gravel, poorly graded sand with silt, poorly graded gravel with sand, poorly graded gravel with silt, well graded gravel with sand, and well graded gravel with silt and sand (USCS: SP, SP-SM, GP, GP-GM, GW, and GW-GM, respectively). The lower sands and gravels were encountered in a medium dense to dense and moist to wet condition. Where encountered, the gravel deposits were observed at depths ranging between three and five feet below existing grades. Intermittent silt lensing was observed in all test pit locations, with exception to test pit locations TP-7 and TP-8, at depths ranging between two and one-half to seven feet bgs.

#### **Geologic Setting**

The referenced geologic map resource indicates the subject site and surrounding area are underlain by Vashon till (Qvt). The referenced WSS resource identifies arents of Alderwood material (Map Unit Symbol: AmB) across the site and surrounding areas. "Arents" refers to Alderwood soils that, despite possible historic disturbance from urban development, retain many features of Alderwood soils, which were formed in till plains. Based on the conditions encountered during our subsurface exploration, native site soils are more consistent with the typical make-up of Vashon recessional outwash deposits.

Earth Solutions NW. LLC

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#### Groundwater

Light groundwater seepage was encountered at test pit location TP-2 at a depth of eight feet bgs and test pit location TP-6 at a depth of six and one-half feet bgs during our May 2019 exploration. It should be noted seepage rates and elevations fluctuate depending on many factors, including precipitation duration and intensity, the time of year, and soil conditions. In general, groundwater flow rates are higher during the wetter, winter months.

#### Infiltration Evaluation

Our evaluation of the proposed infiltration facilities was completed in general accordance with applicable requirements and procedures of the referenced 2014 Washington State Department of Ecology Stormwater Management Manual for Western Washington (2014 SWMMWW) as adopted by the City of Mercer Island. We understand individual infiltration facilities are proposed for each of the four lots on the property.

In-situ testing was completed in general accordance with the small-scale Pilot Infiltration Test (PIT) procedure, as outlined in Section 3.3.6 of Volume III of the 2014 SWMMWW. To evaluate the infiltration capacity of soils, in-situ testing was completed at TP-1 and TP-2 at a depth of three feet bgs and at TP-5, TP-6, and TP-7 at a depth of five feet bgs. Our testing program consisted of a soak period, steady state period, and falling head period. Due to the soil variability across the property, three separate preliminary infiltration rates were calculated for the predominant soil types observed at the property (silty sand, cleaner sand deposits, and gravels). The table below summarizes the short-term (measured) rate at each test location, in units of inches per hour (iph).

Test Pit	Measured Rate (iph)	Depth (feet)	Soil Type
TP-1, TP-2, & TP-6	1	3	Silty sand (SM)
TP-5	13.5	5	Poorly graded sand with silt (SP-SM)
TP-7	18.5	5	Well graded gravel with sand (GW)

Per the referenced 2014 SWMMWW, correction factors must be applied to the measured rates to account for site variability, testing methods, and influent control to prevent siltation. In our opinion, the following correction factors and calculated total correction factor should be applied to the measured field rates.

•	CF <sub>v</sub> (site variability; number of tests)	0.33
•	CFt (test method)	0.5
•	CF <sub>m</sub> (degree of fluent control)	0.9
•	CFt (total correction factor)	0.15

Earth Solutions NW, LLC

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Application of the total correction factor to the measured rates are provided in the table below:

Test Pit	Design Rate (iph)
TP-1, TP-2, & TP-6	0.15
TP-5	2.03
TP-7	2.78

From a geotechnical standpoint, infiltration is feasible within locations underlain by gravels and clean sand deposits. The silty sand deposits identified at the property generally exhibit poor infiltration potential and should not be targeted for infiltration facilities. Minimum vertical separation between the bottoms of the proposed facilities and groundwater must be considered during design. We recommend provisions for overflow be incorporated into final designs, wherever practicable.

Given the variability of the site soils infiltration potential, ESNW should be in correspondence with the facility designer to assist with applying appropriate rates to the targeted infiltrating soils at each proposed lot, acknowledging depth to restrictive layers, and identifying appropriate facility locations per each lot. Additionally, ESNW should be retained at the time of facility construction to confirm soils types and provide additional recommendations as needed.

#### **Limitations**

This letter has been prepared for the exclusive use of RKK Construction, Inc. and their representatives. A warranty is neither expressed nor implied. The recommendations and conclusions provided in this letter are professional opinions consistent with the level of care and skill that is typical of other members in the profession currently practicing under similar conditions in this area. Variations in the soil and groundwater conditions encountered at the test pit locations may exist and may not become evident until construction. ESNW should reevaluate the contents of this letter if variations are encountered. ESNW should be retained during construction to observe facility installation and to confirm soil types are as anticipated in this letter. Supplementary recommendations may be provided during construction, as necessary.

ES-6695 Page 5

We appreciate the opportunity to be of service to you and trust this letter meets your current needs. Should you have questions, or if additional information is required, please call.

Sincerely,

EARTH SOLUTIONS NW, LLC

Kyler T. Kelly Staff Geologist

Raymond A. Coglas, P.E. Principal Engineer

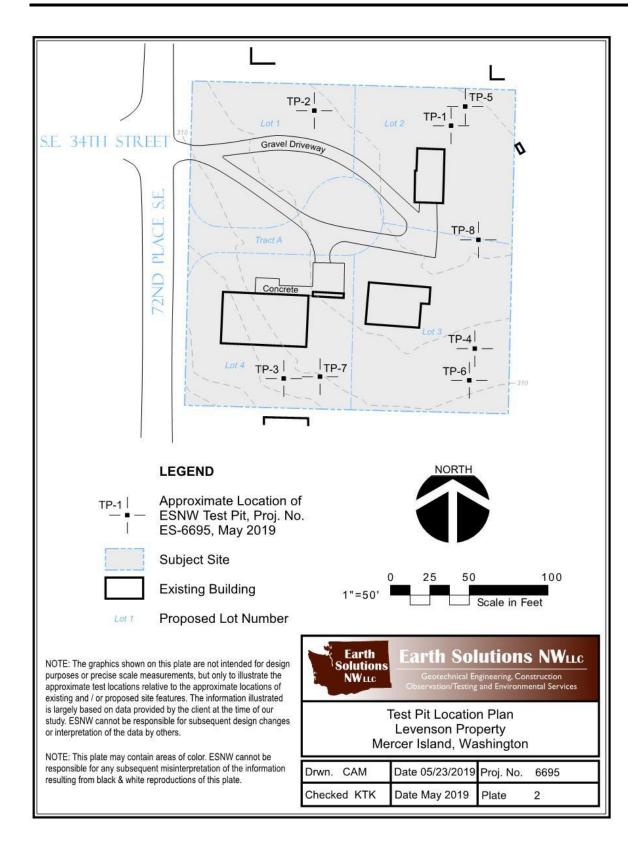
Attachments: Plate 1 - Vicinity Map

Plate 2 - Test Pit Location Plan

Test Pit Logs

Grain Size Distribution





# Earth Solutions NWLLC SOIL CLASSIFICATION CHART

	A IOD DIVISI	ONE	SYMI	BOLS	TYPICAL
IV.	AJOR DIVISI	UNS		LETTER	DESCRIPTIONS
	GRAVEL AND	CLEAN GRAVELS		GW	WELL-GRADED GRAVELS, GRAVEL- SAND MIXTURES, LITTLE OR NO FINES
	GRAVELLY SOILS	(LITTLE OR NO FINES)		GP	POORLY-GRADED GRAVELS, GRAVEL - SAND MIXTURES, LITTLE OR NO FINES
COARSE GRAINED SOILS	MORE THAN 50% OF COARSE	GRAVELS WITH FINES		GM	SILTY GRAVELS, GRAVEL - SAND - SILT MIXTURES
	FRACTION RETAINED ON NO. 4 SIEVE	(APPRECIABLE AMOUNT OF FINES)		GC	CLAYEY GRAVELS, GRAVEL - SAND - CLAY MIXTURES
MORE THAN 50% OF MATERIAL IS	SAND AND	CLEAN SANDS		sw	WELL-GRADED SANDS, GRAVELLY SANDS, LITTLE OR NO FINES
LARGER THAN NO. 200 SIEVE SIZE	SANDY SOILS	(LITTLE OR NO FINES)	$\times$	SP	POORLY-GRADED SANDS, GRAVELLY SAND, LITTLE OR NO FINES
	MORE THAN 50% OF COARSE FRACTION	SANDS WITH FINES		SM	SILTY SANDS, SAND - SILT MIXTURES
	PASSING ON NO. 4 SIEVE	(APPRECIABLE AMOUNT OF FINES)		sc	CLAYEY SANDS, SAND - CLAY MIXTURES
				ML	INORGANIC SILTS AND VERY FINE SANDS, ROCK FLOUR, SILTY OR CLAYEY FINE SANDS OR CLAYEY SILTS WITH SLIGHT PLASTICITY
FINE GRAINED SOILS	SILTS AND CLAYS	LIQUID LIMIT LESS THAN 50		CL	INORGANIC CLAYS OF LOW TO MEDIUM PLASTICITY, GRAVELLY CLAYS, SANDY CLAYS, SILTY CLAYS, LEAN CLAYS
30123				OL	ORGANIC SILTS AND ORGANIC SILTY CLAYS OF LOW PLASTICITY
MORE THAN 50% OF MATERIAL IS SMALLER THAN NO. 200 SIEVE				МН	INORGANIC SILTS, MICACEOUS OR DIATOMACEOUS FINE SAND OR SILTY SOILS
SIZE	SILTS AND CLAYS	LIQUID LIMIT GREATER THAN 50		СН	INORGANIC CLAYS OF HIGH PLASTICITY
				ОН	ORGANIC CLAYS OF MEDIUM TO HIGH PLASTICITY, ORGANIC SILTS
н	GHLY ORGANIC	SOILS	70 70 70 70 \$ 40 70 40 40 40 40 40 40	PT	PEAT, HUMUS, SWAMP SOILS WITH HIGH ORGANIC CONTENTS

DUAL SYMBOLS are used to indicate borderline soil classifications.

The discussion in the text of this report is necessary for a proper understanding of the nature of the material presented in the attached logs.

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DATE STARTE EXCAVATION O EXCAVATION I LOGGED BY NOTES Depth	METHOD	CHI	ECKED	, Inc. GROUND WATER LEVELS:	
O DEPTH (ft) SAMPLE TYPE NUMBER	TESTS	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	
25 To 100	MC = 11.20%  MC = 12.10%  Fines = 20.60%  MC = 11.60%  MC = 17.80%  Fines = 9.20%	SM SP-SM		Brown silty SAND, loose, moist  -becomes medium dense -infiltration test at 3', caving to BOH [USDA Classification: slightly gravelly loamy SAND]  Brown poorly graded SAND with silt, medium dense, wet -intermittent silt lenses from 4' to 6'  -small root intrusions  [USDA Classification: slightly gravelly SAND]  Test pit terminated at 8.5 feet below existing grade. No groundwater encountered during excavation. Caving observed from 3.0 feet to BOH.  Bottom of test pit at 8.5 feet.	311.

Dark brown TOPSOIL, trace roots to 2.5' (Fill) -ceramic debris	So	lutions Bellevue, Wa	Place N.E., So ashington 9800 425-449-4704	05	TEST PIT NUMBER TP	
EXCAVATION CONTRACTOR RKK Construction, Inc.  EXCAVATION METHOD  AT TIME OF EXCAVATION  AT END OF EXCAVATION	PROJECT	NUMBER ES-6695			PROJECT NAME Levenson Property	
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-minor caving to BOH  -minor caving to BOH  -small root intrusions  8.0  Brown poorly graded SAND with gravel, dense, saturated -light groundwater seepage at 8' [USDA Classification: extremely gravelly coarse SAND]  Test pit terminated at 9.0 feet below existing grade. Groundwater seepage encountered at 8.0 feet during excavation. Caving observed from 6.0 feet to BOH.				-small root intr	usions	
- small root intrusions  8.0  SP  Brown poorly graded SAND with gravel, dense, saturated -light groundwater seepage at 8' [USDA Classification: extremely gravelly coarse SAND]  Test pit terminated at 9.0 feet below existing grade. Groundwater seepage encountered at 8.0 feet during excavation. Caving observed from 6.0 feet to BOH.	-			-minor caving	to BOH	
-small root intrusions  30  Brown poorly graded SAND with gravel, dense, saturated -light groundwater seepage at 8' [USDA Classification: extremely gravelly coarse SAND]  Test pit terminated at 9.0 feet below existing grade. Groundwater seepage encountered at 8.0 feet during excavation. Caving observed from 6.0 feet to BOH.		140 17 100/		3		
Brown poorly graded SAND with gravel, dense, saturated -light groundwater seepage at 8' [USDA Classification: extremely gravelly coarse SAND]  Test pit terminated at 9.0 feet below existing grade. Groundwater seepage encountered at 8.0 feet during excavation. Caving observed from 6.0 feet to BOH.	1	MC = 17.40%		-small root intr	usions	
MC = 9.60% Fines = 3.20%  SP  -light groundwater seepage at 8"  [USDA Classification: extremely gravelly coarse SAND]  Test pit terminated at 9.0 feet below existing grade. Groundwater seepage encountered at 8.0 feet during excavation. Caving observed from 6.0 feet to BOH.	-		11118	Brown noorly o	graded SAND with gravel, dense, saturated	306.
Fines = 3.20%  Test pit terminated at 9.0 feet below existing grade. Groundwater seepage encountered at 8.0 feet during excavation. Caving observed from 6.0 feet to BOH.		MC = 9.60%		-light groundw	ater seepage at 8'	305.
		Fines = 3.20%		Test pit termin	ated at 9.0 feet below existing grade. Groundwater seepage encountered ng excavation. Caving observed from 6.0 feet to BOH.	

Solutio NW	DIS Bellevue, W	h Place /ashingt 425-44	N.E., S on 980 9-470		
	BER ES-6695		C 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	PROJECT NAME _Levenson Property	
	D 5/8/19 CONTRACTOR RK			ED 5/8/19         GROUND ELEVATION 309 ft         TEST PIT SIZE           Inc.         GROUND WATER LEVELS:	
				AT TIME OF EXCAVATION	
Marie Services - 1886	CHECKS DOLONGS TO TO SERVE	These out		BY HTW AT END OF EXCAVATION	
	of Topsoil & Sod 6"	-12": gr	ass	AFTER EXCAVATION	
SAMPLE TYPE NUMBER	TESTS	U,S,C.S,	GRAPHIC	MATERIAL DESCRIPTION	
0		TDSI	24 7	Dark brown TOPSOIL, trace roots to BOH	
-		IPSL	2 <u>22</u>	.0  Brown silty SAND, medium dense, moist	308
	MC = 11.90%	SM		-increased gravel content -intermittent silt lenses to 6'	
5			040	Gray poorly graded GRAVEL with silt, dense, moist	304
-	MC = 7.60%	GP- GM	( ) little	-caving from 5' to BOH	302
-	MC = 4.30%	GP		Gray poorly graded GRAVEL with sand, dense, moist	50,
	MC = 5.40%		000	Test pit terminated at 8.5 feet below existing grade. No groundwater encountered during excavation. Caving observed from 5.0 feet to BOH.  Bottom of test pit at 8.5 feet.	30 g

Solutio NWu	Earth Soluti 1805 - 136t Bellevue, W Telephone: Fax: 425-4	h Place /ashingt 425-44	N.E., Suit ton 98005 19-4704	e 201	TEST PIT NUMBER TE	
JECT NUM	BER ES-6695				PROJECT NAME Levenson Property	
	5/8/19				GROUND ELEVATION 312 ft TEST PIT SIZE	
					GROUND WATER LEVELS:	
	METHOD				AT TIME OF EXCAVATION	
GED BY _				/ HTW		
ES Depth	of Topsoil & Sod 12	grass	S		AFTER EXCAVATION	
SAMPLE TYPE NUMBER	TESTS	U.S.C.S.	GRAPHIC LOG		MATERIAL DESCRIPTION	
		TPSL	4 14 1		PSOIL, trace roots to 6'	244
1			1.0	Brown silty SAI	ND, medium dense, moist	311.0
1	MC = 8.70%	2000				
		SM		-becomes dens	e, intermittent silt lenses to 6'	
-			3.5	in account of account		308.
]	MC = 6.90%		000		raded GRAVEL with sand, dense, moist	500
1	MC = 6.90%		601			
- 1		0.0	000	minor caulng t	BOH	
		GP	60	-minor caving to	3 BON	
1			.0°			
	MC = 7.80%		0 7.0			305.0
		58850	$\Lambda\Lambda$	Gray poorly gra	ded SAND with gravel, dense, moist	
		SP	M.		4	
	MC = 13.00%		8.5	Test pit termina excavation. Car	sted at 8.5 feet below existing grade. No groundwater encountered during ving observed from 5.0 feet to BOH.  Bottom of test pit at 8.5 feet.	303.

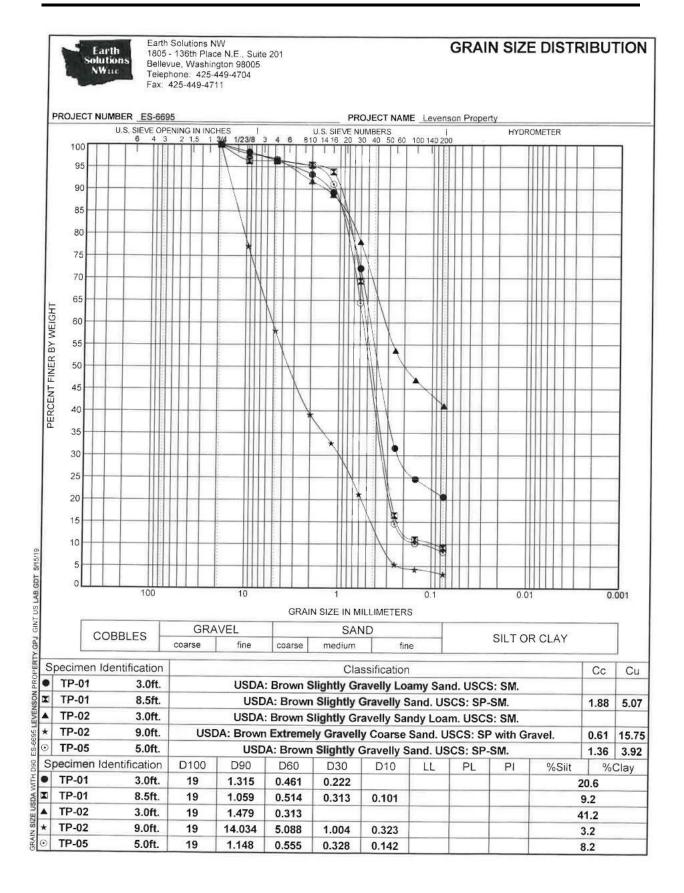
GENERAL BH / TP / WELL 6695,GPJ GINT US,GDT 5/24/19

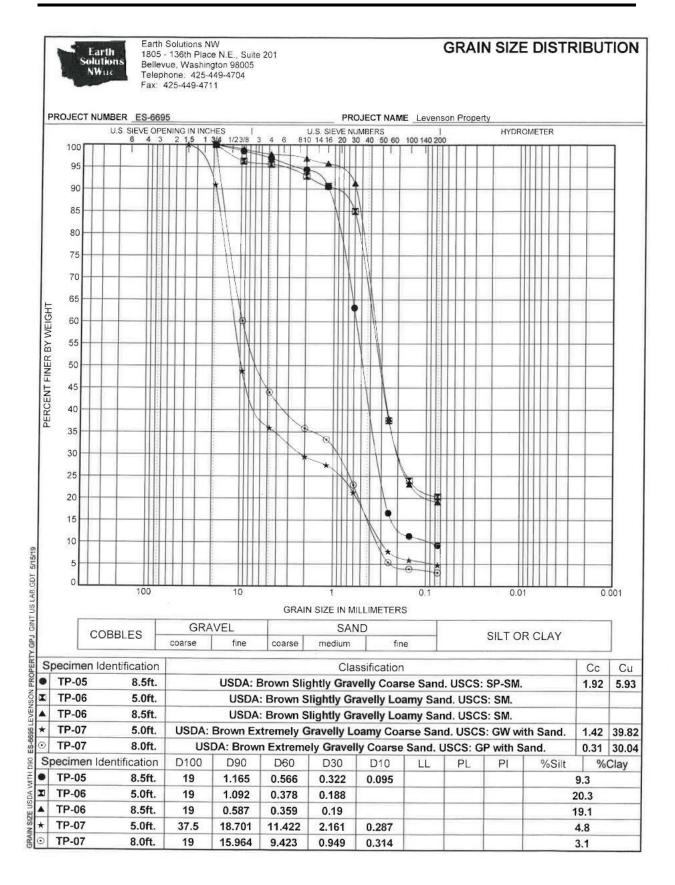
Ì	Eart Soluti NW	DIIS Bellevue, W	n Place ashingt 425-44	N.E., on 980 9-470	005 PAGE 1 0	
DATE EXCA EXCA LOGG	STARTE VATION ( VATION I ED BY	CONTRACTOR RK	K Consi	ECKE	PROJECT NAME Levenson Property  TED 5/8/19	
O DEPTH	SAMPLE TYPE NUMBER	TESTS	U.S.C.S.	GRAPHIC		
			TPSL		Dark brown TOPSOIL, trace roots to BOH (Fill)  -plastic debris  Brown silty SAND with gravel, medium dense, moist	315.0
		MC = 14.00%	SM		-intermittent silt lenses to 6'	312.0
5		MC = 9.20% Fines = 8.20% MC = 11.70%	SP- SM		Brown poorly graded SAND with silt, dense, moist  -infiltration test at 5' [USDA Classification: slightly gravelly SAND]	
		MC = 11.80% Fines = 9.30%			[USDA Classification: slightly gravelly coarse SAND]  Test pit terminated at 8.5 feet below existing grade. No groundwater encountered during excavation. No caving observed.  Bottom of test pit at 8.5 feet.	307.5

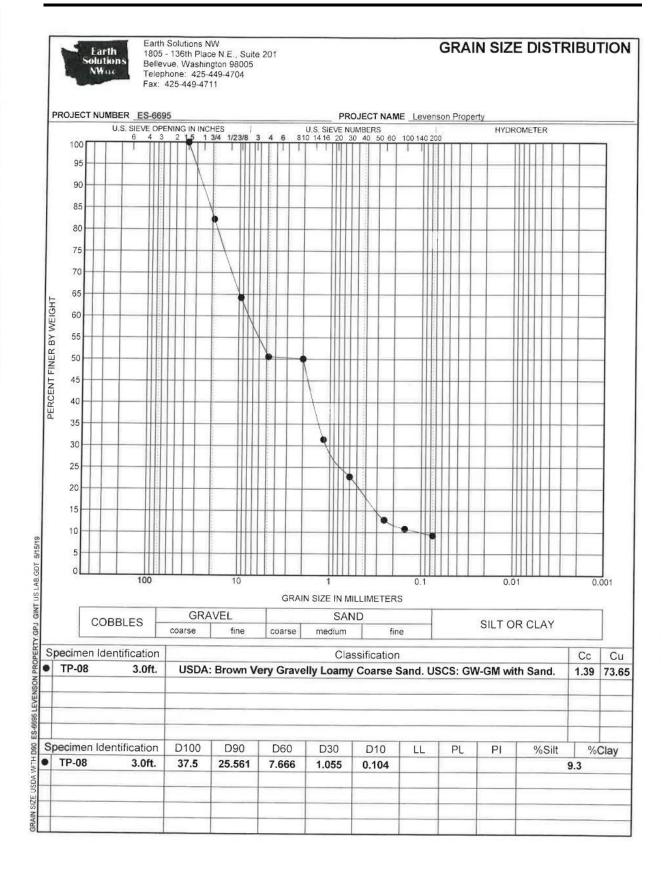
PROJECT NUMBER ES-6695  PROJECT NUMBER Levenson Property  DATE STARTED 5/8/19  COMPLETED 5/8/19  GROUND BLEVATION 310 ft TEST PIT SIZE  EXCAVATION CONTRACTOR RKK Construction, Inc.  EXCAVATION METHOD  LOGGED BY KTK  CHECKED BY HTW  AT TIME OF EXCAVATION  AT TI	
AT END OF EXCAVATION   AFTER E	
Dark brown TOPSOIL, trace roots to 7.5'  MC = 14.90%  MC = 17.40% Fines = 20.30% MC = 20.30% MC = 17.40% MC = 17.40% MC = 17.40% MC = 19.90% Fines = 19.10%  Dark brown TOPSOIL, trace roots to 7.5'  Brown silty SAND, medium dense, moist  -becomes dense, intermittent silt lenses to 6.5'  [USDA Classification: slightly gravelly loamy SAND]	
Dark brown TOPSOIL, trace roots to 7.5'  TPSL  MC = 14.90%  MC = 17.40% Fines = 20.30%  MC = 20.30%  MC = 17.40%  MC = 17.40%  MC = 19.90%  Fines = 19.10%  MC = 19.90% Fines = 19.10%  MC = 19.90% Fines = 19.10%  MC = 19.90% Fines = 19.10%  MC = 19.90% Fines = 19.10%  Test pit terminated at 8.5 feet below existing grade. Groundwater seepage encour at 6.5 feet during excavation. Caving observed from 6.0 feet to BOH.	02200
Brown silty SAND, medium dense, moist  MC = 17.40% Fines = 20.30%  MC = 20.30%  MC = 20.30%  MC = 17.40%  MC = 17.40%  MC = 17.40%  MC = 19.90% Fines = 19.10%  Brown silty SAND, medium dense, moist  -becomes dense, intermittent silt lenses to 6.5'  [USDA Classification: slightly gravelly loamy SAND] -infiltration test at 5' -becomes wet -minor caving to BOH -light groundwater seepage  [USDA Classification: slightly gravelly loamy SAND]  Test pit terminated at 8.5 feet below existing grade. Groundwater seepage encour at 6.5 feet during excavation. Caving observed from 6.0 feet to BOH.	
MC = 17.40% Fines = 20.30%  MC = 20.30%  MC = 17.40%  MC = 17.40%  MC = 19.90% Fines = 19.10%	309.0
Fines = 20.30%  MC = 20.30%  MC = 17.40%  MC = 19.90% Fines = 19.10%  Fines = 19.10%  [USDA Classification: slightly gravelly loamy SAND]  - Ight groundwater seepage  [USDA Classification: slightly gravelly loamy SAND]  Test pit terminated at 8.5 feet below existing grade. Groundwater seepage encour at 6.5 feet during excavation. Caving observed from 6.0 feet to BOH.	
- Ight groundwater seepage  MC = 17.40%  MC = 19.90% Fines = 19.10%  MC = 19.10%  MC = 19.00% Fines = 19.10%  Test pit terminated at 8.5 feet below existing grade. Groundwater seepage encour at 6.5 feet during excavation. Caving observed from 6.0 feet to BOH.	
Fines = 19.10%  Test pit terminated at 8.5 feet below existing grade. Groundwater seepage encour at 6.5 feet during excavation. Caving observed from 6.0 feet to BOH.	
Fines = 19.10%  Test pit terminated at 8.5 feet below existing grade. Groundwater seepage encour at 6.5 feet during excavation. Caving observed from 6.0 feet to BOH.	301.5
95	
200	
GENERAL BH / TP / WELL 6695, GPJ GINT US; GDT 5/30/19	

Eart Soluti NW	Ons Bellevue, W	h Place N lashingto 425-449		TEST PIT NUMBER TP-
PROJECT NUM	IBER ES-6695			PROJECT NAME Levenson Property
			PLETED 5/8/19	GROUND ELEVATION 310 ft TEST PIT SIZE
				GROUND WATER LEVELS:
	KTK of Topsoil & Sod 12		CKED BY HTW	AFTER EXCAVATION
	101 10p30ii u 00u 12	T T		A LEN ENGLANDIN
SAMPLE TYPE	TESTS	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION
0		TDCI	Dark bro	wn TOPSOIL, trace roots to 7'
_		TPSL	1.0	30
		SM	Brown si	lty SAND with gravel, medium dense, moist
-		J SIVI	2.5	30
	MC = 8.10%	SP-		porly graded SAND with silt, medium dense, moist
		SM	3.5 Brown w	ell-graded GRAVEL with sand, dense, moist
-			A. Diotim	Sir graded of Vivie Harroand, across, mode
5_	MC = 5.70%	GW .		
	Fines = 4.80%			on test at 5' Classification: extremely gravelly loamy coarse SAND]
-	MC = 7.90%	-	Brown po	porly graded GRAVEL with sand, dense, moist
			0	F POT SEE BOOMSON
1 1		Oi I	Od -moderat	te caving to BOH
	MC = 9.50% Fines = 3.10%		Test pit t	classification: extremely gravelly coarse SAND]  erminated at 8.0 feet below existing grade. No groundwater encountered during on. Caving observed from 7.0 feet to BOH.  Bottom of test pit at 8.0 feet.

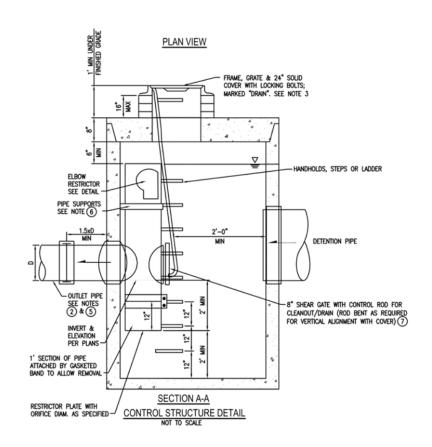
Soluti NW	Ons Bellevue W	h Place Vashingto 425-44	N.E., Suite on 98005 9-4704	TEST PIT NUMBER TP- PAGE 1 OF
	IBER ES-6695			PROJECT NAME Levenson Property
ATE STARTE		10000	MPLETED	**************************************
	CAVATION CONTRACTOR RKK Construction, Inc.  CAVATION METHOD			AT TIME OF EXCAVATION
OGGED BY _	ED BY KTK CHECKED BY HTW		CKED BY	HTW AT END OF EXCAVATION
OTES Depth	of Topsoil & Sod 6"	': grass		AFTER EXCAVATION
SAMPLE TYPE NUMBER	TESTS	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION
0		TPSL	37 30.5	Dark brown TOPSOIL, trace roots to BOH
_				Brown silty SAND with gravel, medium dense, moist
	MC = 5.40% Fines = 9.30%	SM	3.0	
		GW- GM		Brown well-graded GRAVEL with silt and sand, dense, moist -moderate caving from 3' to BOH [USDA Classification: very gravelly loamy coarse SAND] -increased gravel and cobble size
	MC = 3.10%		6.0	Test pit terminated at 6.0 feet below existing grade due to caving. No groundwater encountered during excavation. Caving observed from 3.0 feet to BOH.  Bottom of test pit at 6.0 feet.



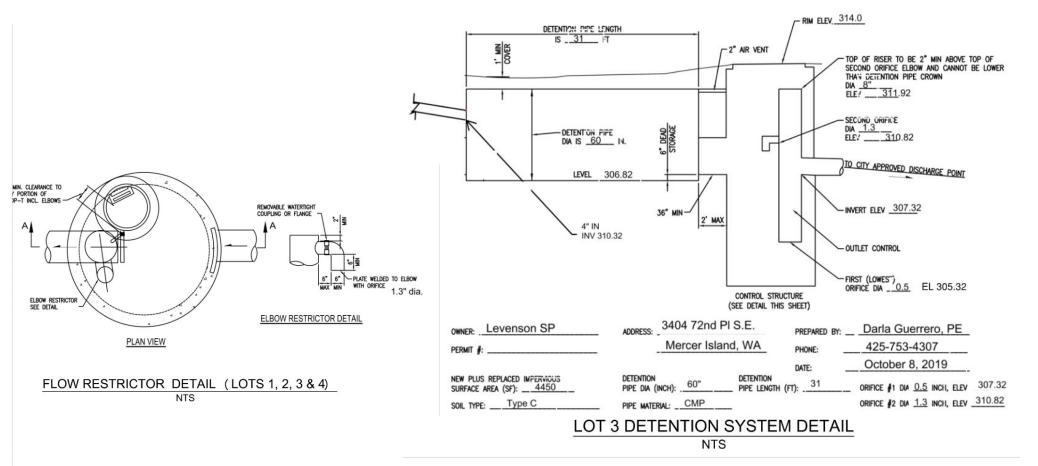




### **Appendix B: Detention Design**



TYPICAL 60"Ø FLOW CONTROL STRUCTURE DETAIL NTS



#### **ON-SITE DETENTION SYSTEM NOTES:**

- 1. CALL DEVELOPMENT SERVICES (206-275-7605) 24 HOURS IN ADVANCE FOR A DETENTION SYSTEM INSPECTION BEFORE BACKFILLING AND FOR FINAL INSPECTIONS.
- 2. RESPONSIBILITY FOR OPERATION AND MAINTANANCE OF DRAINAGE SYSTEMS ON PRIVATE PROPERTY IS RESPONSIBILITY OF THE PROPERTY OWNER. MATERIAL ACCUMULATED IN THE STORAGE PIPE MUST BE REMOVED FROM CATCH BASINS TO ALLOW PROPER OPERATION. THE OUTLET CONTROL ORIFICE MUST BE KEPT OPEN AT ALL TIMES.
- 3. PIPE MATERIAL, JOINT, AND PROTECTIVE TREATMENT SHALL BE IN ACCORDANCE WITH SECTION 7.04 AND 9.05 OF THE WSDOT STANDARD SPECIFICATION FOR ROAD, BRIDGE, AND MUNICIPAL CONSTRUCTION, LATEST VERSION. SUCH MATERIALS INCLUDE THE FOLLOWING, LINED CORRUGATED POLYETHYLENE PIPE (LCPE), ALUMINIZED TYPE 2 CORRUGATED STEEL PIPE AND PIPE ARCH (MEETS AASHTO DESIGNATIONS M274 AND M36), CORRUGATED OR SPIRAL RIB ALUMINUM PIPE, OR REINFORCED CONCRETE PIPE. CORRUGATED STEEL PIPE IS NOT ALLOWED.
- 4. FOOTING DRAINS SHALL NOT BE CONNECTED TO THE DETENTION SYSTEM.

#### CONTROL STRUCTURE NOTES:

- 1) USE A MINIMUM OF A 54 IN. DIAM. TYPE 2 CATCH BASIN. THE ACTUAL SIZE IS DEPENDENT ON CONNECTING PIPE MATERIAL AND DIAMETER.
- 2) OUTLET PIPE: MIN. 6 INCH.
- (3) METAL PARTS: CORROSION RESISTANT, NON-GALVANIZED PARTS PREFERRED, GALVANIZED PIPE PARTS TO HAVE ASPHALT TREATMENT 1.
- (4) FRAME AND LADDER OR STEPS OFFSET SO:
  - A. CLEANOUT GATE IS VISIBLE FROM TOP:
  - B. CLIMB-DOWN SPACE IS CLEAR OF RISER AND CLEANOUT GATE;
  - C. FRAME IS CLEAR OF CURB.
- CONCRETE PIPE I.D. LESS 1/4 IN.
- 6 PROVIDE AT LEAST ONE 3 X 0.090 GAUGE SUPPORT BRACKET ANCHORED TO CONCRETE WALL WITH 5/8 IN. STANLESS STEEL EXPANSION BOLTS OR EMBEDDED SUPPORTS 2 IN. INTO CATCH BASIN WALL (MAXIMUM 3'-0" VERTICAL SPACING).
- THE SHEAR GATE SHALL BE MADE OF ALUMINUM ALLOY IN ACCORDANCE WITH ASTM B 26M AND ASTM B 275, DESIGNATION ZG32A; OR CAST IRON IN ACCORDANCE WITH ASTM A 48, CLASS 30B. THE LIFT HANDLE SHALL BE MADE OF A SIMILAR METAL TO THE GATE (TO PREVENT GALVANIC CORROSION), IT MAY BE OF SOLID ROD OR HOLLOW TUBING, WITH ADJUSTABLE HOOK AS REQUIRED.

  A NEOPRENE RUBBER GASKET IS REQUIRED BETWEEN THE RISER MOUNTING FLANGE AND THE GATE FLANGE. INSTALL THE GATE SO THAT THE LEVEL-LINE MARK IS LEVEL WHEN THE GATE IS CLOSED. THE MATING SURFACES OF THE LID AND THE BODY SHALL BE MACHINED FOR PROPER FIT. ALL SHEAR GATE BOLTS SHALL BE STAINLESS STEEL.
- (5) IF METAL OUTLET PIPE CONNECTS TO CEMENT CONCRETE PIPE, OUTLET PIPE TO HAVE SMOOTH O.D. EQUAL TO (8) THE UPPER CATCH BASIN IS REQUIRED IF THE LENGTH OF THE DETENTION PIPE IS GREATER THAN 50 FT.

### **Appendix C: Operations and Maintenance Manual**

#### Table V-4.5.2(16) Maintenance Standards · Oil/Water Separators

Maintenance Component	Detect	Condition When Main- tenance is Needed	Results Expected When Maintenance is Performed
	Monitoring	Inspection of discharge water for obvious signs of poor water quality.	Effluent discharge from vault should be clear with out thick visible sheen.
General	Sediment Accu- mulation	Sediment depth in bottom of vault exceeds 6-inches in depth.	No sediment deposits on vault bottom that would impede flow through the vault and reduce separation efficiency.
	Trash and Debris Accumulation	Trash and debris accu- mulation in vault, or pipe inlet/outlet, floatables and non-floatables.	Trash and debris removed from vault, and inlet/outlet piping.
	Oil Accumulation	Oil accumulations that exceed 1-inch, at the surface of the water.	Extract oil from vault by vactoring. Disposal in accordance with state and local rules and reg ulations.
Maintenance Component	Detect	Condition When Main- tenance is Needed	Results Expected When Maintenance is Performed
	Damaged Pipes	Inlet or outlet piping dam- aged or broken and in need of repair.	Pipe repaired or replaced.
	Access Cover Damaged/Not Working	Cover cannot be opened, corrosion/deformation of cover.	Cover repaired to proper working specifications or replaced.
	Vault Structure Damage - Includes Cracks in Walls Bot	See "Catch Basins" (No. 5) Cracks wider than 1/2-inch at the joint of any inlet/outlet	Vault replaced or repairs made so that vault meets design specifications and is structurally sound.
	tom, Damage to Frame and/or Top Slab	pipe or evidence of soil particles entering through the cracks.	Vault repaired so that no cracks exist wider than 1/4-inch at the joint of the inlet/outlet pipe.

Table V-4.5.2(5) Maintenance Standards - Catch Basins

Maintenance Component	Defect	Conditions When Maintenance is Needed	Results Expected When Main- tenance is performed
General	Trash & Debris	Trash or debris which is located immediately in front of the catch basin opening or is blocking inletting capacity of the basin by more than 10%.  Trash or debris (in the basin) that exceeds 60 percent of the sump depth as measured from the bottom of basin to invert of the lowest pipe into or out of the basin, but in no case less than a minimum of six inches clearance from the debris surface to the invert of the lowest pipe.  Trash or debris in any inlet or outlet pipe blocking more than 1/3 of its height.  Dead animals or vegetation that could generate odors that could cause complaints or dangerous gases (e.g., methane).	No Trash or debris located immediately in front of catch basin or on grate opening.  No trash or debris in the catch basin. Inlet and outlet pipes free of trash or debris.  No dead animals or vegetation present within the catch basin.
	Sediment	Sediment (in the basin) that exceeds 60 percent of the sump depth as measured from the bottom of basin to invert of the lowest pipe into or out of the basin, but in no case less than a minimum of 6 inches clearance from the sediment surface to the invert of the lowest pipe.	No sediment in the catch basin
	Structure Damage to Frame and/or Top Slab	Top slab has holes larger than 2 square inches or cracks wider than 1/4 inch. (Intent is to make sure no material is running into basin).	Top slab is free of holes and cracks. Frame is sit-

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Table V-4.5.2(5) Maintenance Standards - Catch Basins (continued)

Maintenance Component	Detect	Conditions When Maintenance is Needed	Results Expected When Main- tenance is performed
		Frame not sitting flush on top slab, i.e., separation of more than 3/4 inch of the frame from the top slab. Frame not securely attached	ting flush on the riser rings or top slab and firmly attached.
	Fractures or Cracks in Basin Walls/ Bottom	Grout fillet has separated or cracked wider than 1/2 inch and longer than 1 foot at the joint of any inlet/outlet pipe or any evidence of soil particles entering catch basin through	repaired to design stand ards. Pipe is
	Settlement/ Misalignment	tion, or design problem.	Basin replaced or repaired to design stand ards.
	Vegetation growing across and blocking more than 10% of the basin opening.  Vegetation  Vegetation growing in inlet/outlet pipe joints that is more than six inches tall and less than six inches apart.	No veget- ation block- ing opening to basin. No veget- ation or root growth present.	
	Contamination and Pollution	See "Detention Ponds" (No. 1).	No pollution present.
Catch Basin Cover	Cover Not in Place		Catch basin cover is closed
	Locking Mech- anism Not	Mechanism cannot be opened by one maintenance person with proper tools. Bolts into	Mechanism opens with

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### **Appendix D: Downstream Level One Analysis**

### **NOT REQUIRED**

### **Appendix E: City of Mercer Island Hazard Maps**

